

CIRCUITS AND METHODS
FOR CURRENT MEASUREMENTS
REFERRED TO A PRECISION IMPEDANCE

Background of the Invention

5 This invention relates to driver circuitry.
More particularly, this invention relates to driver
circuitry that performs current measurements using a
precision external resistor.

10 In the past, the semiconductor industry has
utilized various configurations of "driver circuitry" for
supplying power to loads that are external to an integrated
circuit. Common examples of such external loads include
transmission lines, communication systems, electric motors,
and illumination systems. One characteristic of driver
15 circuitry that is of interest to system designers is the
amount of current the driver circuitry actually supplies to
the external load. In certain applications, such as those
involving power transmission or lighting systems, it is not
necessary for the driver circuitry to obtain precise values

of the supplied current. Other applications, however, such as communications systems, often rely on precise bias and modulation current measurements to properly function.

Previously, precision current measurements have been made
5 possible by "trimming" on-chip resistors and voltage references to obtain tolerance values suitable for current sensing. This method, however, is costly and time consuming.

In light of the foregoing, it would therefore be
10 desirable to provide circuits and methods for accurately calculating the current supplied by driver circuitry without resorting to costly and time consuming trimming techniques.

Summary of the Invention

It is therefore an object of the present invention
15 to provide circuits and methods for precisely calculating the current supplied by driver circuitry without resorting to costly and time consuming resistor trimming techniques.

This and other objects are accomplished in accordance with the principles of the present invention by
20 providing circuits and methods for precisely calculating the current supplied by driver circuitry without resorting to costly and time consuming resistor trimming techniques. Current calculations are performed using information from a precision termination resistor and from the ratio
25 relationship of two on-chip resistors. The invention provides a way to obtain accurate current measurements without the use of component trimming.

Brief Description of the Drawings

The above and other objects and advantages of the present invention will be apparent upon consideration of the following detailed description, taken in conjunction with the accompanying drawings, in which like reference characters refer to like parts throughout, and in which:

FIG. 1 is a schematic diagram of a driver circuit constructed in accordance with the principles of the present invention.

10 Fig. 2 is a schematic diagram of another driver circuit constructed in accordance with the principles of the present invention.

Detailed Description of the Invention

FIG. 1 is an illustrative block diagram of a driver circuit 100 constructed in accordance with the principles of the present invention that can be used to obtain accurate measurements of supplied current. Driver circuit 100 includes a sourcing circuit 10, a sense resistor 15, an external termination resistor 25, analog to digital converters 40 and 55, a sinking circuit 45, and a modulation resistor 50.

Transmission line 30 and load 35 represent the external load driven by circuit 100. Capacitor 20 may also be included in circuit 100, if desired. Although other arrangements are possible, the components within dotted line 60 are typically constructed on an integrated circuit device.

As shown in FIG. 1, sourcing circuit 10 provides a substantially constant source current (I_s) to sense

resistor 15, termination resistor 25, and load 35 (through transmission line 30). Sourcing circuit 10 may be any circuit configuration suitable for providing a substantially constant current such as current mirror type bias circuitry.

5 The current supplied to load 35 may be varied by periodically switching sinking circuit 45 ON and OFF, allowing a modulation current (I_M) to pass through it during an ON state, and acting as an open circuit during an OFF state. In some embodiments, sinking circuit 45 may be
10 configured to turn ON and OFF partially to improve response time. Sinking circuit 45 may include any circuitry suitable for switching between ON and OFF states such as a transistor or armature type switch.

 The value of modulation resistor 50 affects the
15 operation of circuit 100 when sinking circuit 45 is switched ON. For example, when sinking circuit 45 turns ON and current flows across modulation resistor 50, the amount of current supplied to load 35 decreases in proportion to the resulting current divider network. Thus, if modulation
20 resistor 50 has a value significantly less than load 35, the amount of current supplied to load 35 (I_L) decreases significantly. On the other hand, if the value of modulation resistor 50 is much greater than load 35 (i.e., a factor of 10 or more), load current I_L will only decrease
25 somewhat. Thus, a circuit designer may select an approximate value for modulation resistor 50 with respect to load 35 to control the current differential applied across it. This allows circuit designers to define the range of current values supplied by circuit 100, such as those

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associated with the transmission of logic "high" or a logic "low," signal to load 35.

Driver circuit 100 will operate without termination resistor 25. However, because transmission
5 line 30 typically has a characteristic impedance similar to, but not perfectly matched with load 35, a portion of the transmitted signal is reflected back to the driver circuit, causing signal distortion. This problem may be corrected, however, by the addition of termination resistor 25 and
10 capacitor 20, which allows current flow when the line voltage changes. These components help to absorb the reflected energy from load 35 so that high speed current cannot circulate back into the load. The present invention takes advantage of the fact that termination resistor 25
15 typically has significantly higher tolerance level than those found on an integrated circuit, usually around $\pm 1\%$, which can be used to obtain accurate current measurements.

Measurement of source current I_s and modulation current I_M is performed using analog-to-digital converters
20 (A/D converters) 40 and 55. This is accomplished by measuring the voltage drop across termination resistor 25, source resistor 15, and modulation resistor 50. The voltage drop across resistor 50 is divided by the voltage drop across resistor 15 and the voltage drop across termination
25 resistor 25 divided by a reference voltage (not shown). These operations produce discrete values. In FIG. 1, these discrete values are depicted as 'data' outputs that are sent from A/D converters 40 and 55 to computational circuitry or software (not shown) that performs the mathematical
30 operations necessary to determine the modulation current I_M

and source current I_S (discussed in more detail below). Such circuitry may include, but is not limited to, a multiplication amplifier, a microprocessor, a programmable logic array, etc.

5 To calculate modulation current I_M , the value of source current I_S must be known. Generally speaking, source current I_S is substantially equal to the current across termination resistor 25 (I_T) when no current flows through capacitor 20. Current will only flow through capacitor 20
10 when the voltage across it changes. Because this occurs only for a very short duration at the instant sourcing circuit 45 switches from ON to OFF (and vice versa), an accurate measurement of source current I_S may be obtained by measuring the voltage drop across precision termination
15 resistor 25.

 A measurement of the termination voltage (i.e., the voltage drop across termination resistor 25) may be used as a first step in determining the value of source current I_S . For example, during operation, A/D converter 40 may
20 take an analog voltage measurement of the termination voltage with respect to a reference voltage (not shown). This measurement, which is represented as X_{TR} , is the termination voltage divided by the reference voltage. Accordingly, the variable X_{TR} is a dimensionless ratio of
25 these two voltages, having a value between 1 and 0 such that:

$$(1) \quad X_{TR} = V_T/V_{REF}$$

Furthermore, it will be appreciated that the termination voltage is equal to the product of the

termination current (I_T) and the termination resistance (R_T). Substituting this relationship into equation (1) gives the following:

$$(2) \quad X_{TR} = (I_T * R_T) / V_{REF}$$

5 Because source current I_S is equivalent to termination current I_T , equation (2) may be re-written as:

$$(3) \quad X_{TR} = (I_S * R_T) / V_{REF}$$

Solving equation (3) for source current I_S gives the following:

10 (4) $I_S = I_T = X_{TR} * V_{REF} / R_T.$

Thus, as demonstrated above, circuit 100 may calculate the sourcing current I_S as a function of precision termination resistor 25. In some embodiments of the present invention, equation 4 may be solved by an external computing
15 device. The input to such a device is obtained from A/D converter 40.

It will be appreciated from the above that the accuracy of the sourcing current calculation is dependent only upon precision termination resistor 25 and an untrimmed
20 internal voltage reference (not shown). Typically, these circuit components have tolerances of $\pm 1\%$ and $\pm 5\%$, respectively. Thus, using the following well-known statistical error equation:

$$(5) \quad E = \sqrt{X^2 + Y^2}$$

where X represents the tolerance of termination resistor 25, and Y represents the tolerance of the voltage reference, it can be seen the accuracy of the source current measurement is approximately $\pm 5\%$. This is a dramatic improvement over conventional systems that rely on measurements based on an untrimmed voltage reference and an untrimmed sense resistor 15. Because these components typically have tolerances of $\pm 5\%$ and $\pm 20\%$, respectively, the overall accuracy of sourcing current measurements is approximately $\pm 20\%$. Thus, the present invention provides sourcing current measurements that are at least four times more accurate than those provided by conventional systems.

The next step in calculating modulation current I_M is to measure the voltage drop across modulation resistor 50 and compare it to the voltage drop across sensing resistor 15. A/D converter 55 accomplishes this and obtains a value for X_{MS} , which is defined by the following:

$$(6) \quad X_{MS} = V_M/V_S$$

where V_M is the voltage across modulation resistor 50 and V_S is the voltage across sensing resistor 15. According to Ohm's Law, each of these voltages are equal to the product of their respective current and resistance. Therefore:

$$(7) \quad V_M = I_M * R_M; \text{ and}$$

$$(8) \quad V_S = I_S * R_S$$

Substituting equations 7 and 8 into equation 6 yields:

$$(9) \quad X_{MS} = (I_M * R_M) / (I_S * R_S)$$

5

Solving equation 9 for modulation current I_M results in the following relationship:

$$(10) \quad I_M = (X_{MS}) * (R_S / R_M) * (I_S)$$

To solve equation 10, a value of I_S must be
10 obtained. By substituting equation 4 into
equation 10, the following expression is derived:

$$(11) \quad I_M = (X_{MS} * R_S / R_M) * (X_{TR} * V_{REF} / R_T)$$

rearranging equation 11 to group like terms, the following
is obtained:

$$15 \quad (12) \quad I_M = (X_{MS} * X_{TR}) (R_S / R_M) (V_{REF} / R_T)$$

Thus, it can be seen from equation 12, that the
measurement of modulation current I_M depends only on the
reference voltage (V_{REF}), termination resistor 25, and the
20 ratio of modulation resistor 50 to sensing resistor 15.
Because existing integrated circuit fabrication techniques
permit the variance of the resistor ratio to be less than

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±1%, the overall accuracy of the modulation current calculation remains approximately ±5%, without the use of trimming. This is a significant improvement over conventional measurement techniques which yield an overall
5 accuracy of about ±20%.

Although driver circuit 100 may be used in a wide variety of applications that involve signal modulation, it is particularly useful for light-based modulation systems. In an optical communication system, for example, it is often
10 necessary to quickly toggle a light source, such as a laser diode, to produce light pulses that are used as communication signals. To do this efficiently, circuit designers usually bias the light source such that it varies between two precise levels. One of the levels represents an
15 optical "logic low," during which a minimum optical signal is produced. The other level represents an optical "logic high" which produces an optical signal of sufficient strength to be differentiated from an optical "logic low" signal. The shorter this dynamic range is, the faster the
20 light source can be varied between a "logic low" and a "logic high." By having accurate measurements of bias and modulation currents, the driver circuitry can determine and optimize the extinction ratio (i.e., the amount of optical power need to produce a logic "high" signal compared to the
25 optical power needed to produce a logic "low") of the light source.

Accurately determining the operating currents and extinction ratio of circuit 100 has many advantages. For example, the average current required to maintain a constant
30 average optical output power provides a good indication of

the operational condition of the light source. For example, the turn ON threshold of a laser diode tends to degrade over time. By monitoring the average laser current, a communications system may accurately predict the imminent failure of the light source and provide a warning about impending failure so replacement can be made without loss of service.

Moreover, accurate measurements of the modulation and bias currents are useful for statistical process control during the final assembly of laser transceiver modules, where accurate measurement of laser setup conditions may give an early indication of manufacturing problems.

Another embodiment of the present invention may be used to calculate the modulation current I_M that also yields an overall accuracy of $\pm 5\%$. This approach is illustrated in FIG. 2 as driver circuit 200 which is similar to driver circuit 100 with the exception that circuit 200 employs a third A/D converter 60. A/D converter 60 measures the voltage drop across sensing resistor 15 with respect to a reference voltage (not shown) and generates a value represented as X_{SR} . A/D converter 55 no longer uses the voltage across sensing resistor 15 as a reference. Next, A/D converter 40 operates as described above and determines X_{TR} . A/D converter 55 then determines X_{MR} , instead of X_{MS} , where X_{MR} is the voltage drop across modulation resistor 50 measured with respect to a reference voltage (not shown) so that:

$$(13) \quad X_{MR} = V_M/V_{REF}$$

Using Ohm's law it can be shown that:

$$(14) \quad X_{MR} = I_M * R_M / V_{REF}$$

Solving for I_M yields:

$$(15) \quad I_M = X_{MR} * V_{REF} / R_M$$

5 X_{SR} may be obtained with A/D converter 60 and expressed using the following relationship:

$$(16) \quad X_{SR} = I_S * R_S / V_{REF}$$

Combining equations 3, 14, and 16 and rearranging gives the following:

10
$$(17) \quad I_M = X_{MR} * (X_{TR} / X_{SR}) * (R_S / R_M) * (V_{REF}) / R_T$$

Thus, it can be seen from equation 17, that the measurement of modulation current I_M depends only on the reference voltage (V_{REF}), termination resistor 25, and the ratio of modulation resistor 50 to sensing resistor 15.

15 The readings obtained from A/D converters 40, 55, and 60 may then be sent to processing circuitry to perform the calculations as described above (not shown). Bias and modulation current information may be used to compute feedback information and the extinction ratio. These values
20 may also be used internally by the driver circuit or externally for statistical analysis.

Persons skilled in the art will recognize that the present invention may be implemented using a variety of

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circuit configurations other than those shown and discussed above. For example, the present invention may employ some trimming on the internal reference voltage to improve its accuracy (e.g., to about $\pm 1\%$). This further improves the
5 accuracy of current measurements.

Moreover, termination resistor 25 need not be external to the integrated circuit, rather it may be fabricated on the integrated circuit and trimmed to the appropriate value. Furthermore, sinking circuit 45 may be
10 replaced by or used in conjunction with a signal source that periodically impedes and allows current flow, thus providing modulation.

The present invention may also use data collecting components other than the A/D converters depicted in FIGS. 1
15 and 2 to implement different embodiments of the present invention. In addition, it will be appreciated that some or all of the resistors shown may be replaced by elements such as synthetic circuit components with impedances having a reactive component rather than elements with purely
20 resistive attributes (e.g., a switched capacitor circuit). All such modifications will be recognized as within the scope of the present invention, which is limited only by the claims that follow.